

Supplements to IGEM TD/1 and PD 8010 - Codified Approach for the Application of Pipeline Risk

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Risk Assessment Issues and the Need for Code Guidance

Quantified Risk Analysis is widely used as a tool for risk management of pipelines, but -

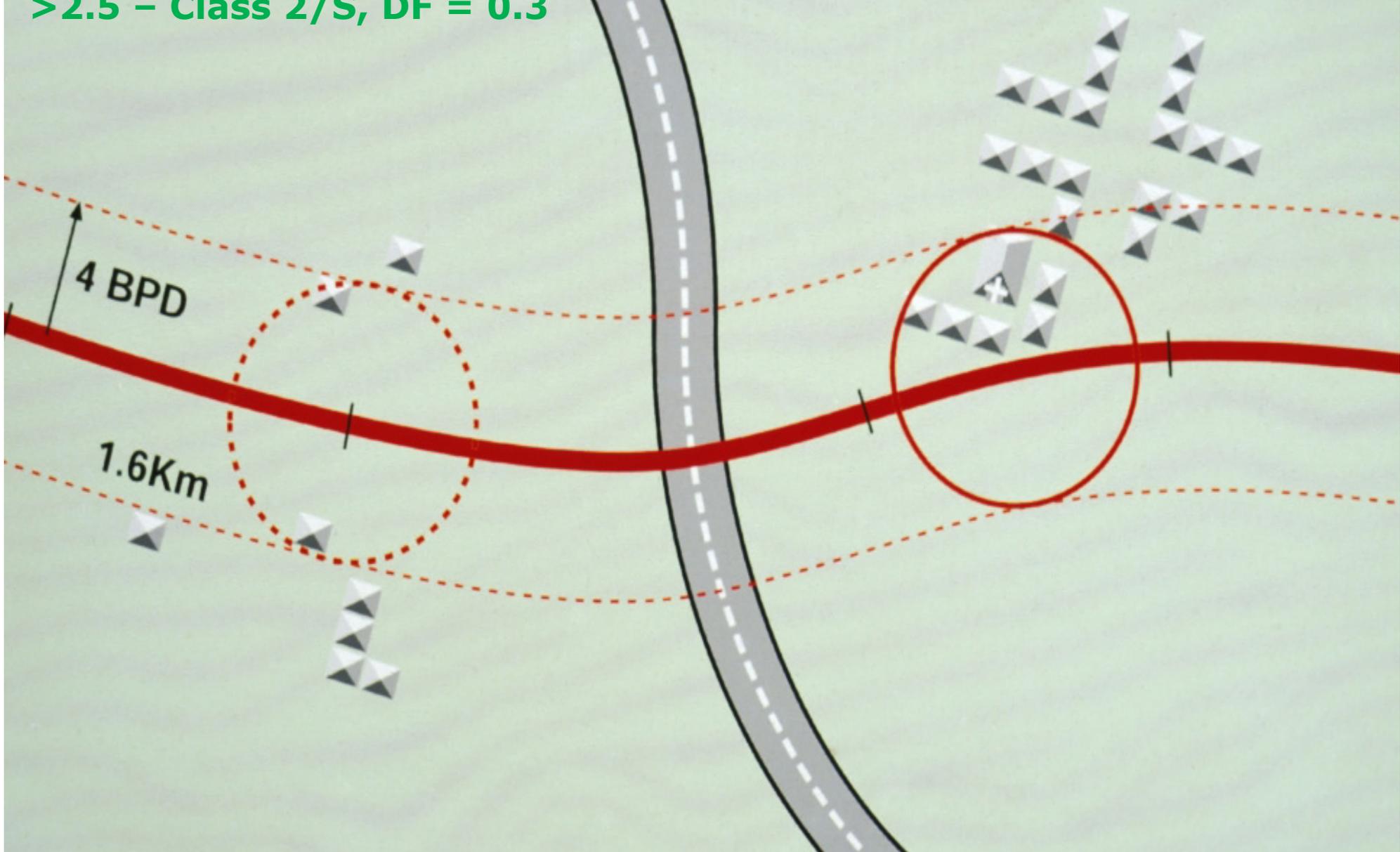
- It is specialist, expert, subject to opinion and disagreement
- Acceptance criteria are not well understood
- UK legislation and codes are risk-based
- HSE use specified risk levels to define LUP zones, and advice is risk based
- Operators, Developers and LA Planners need to assess the risk to proposed developments, and consider how this can be minimised
- Requirement for an agreed methodology for pipeline risk assessment

**Population density
in persons per hectare :-**

≤2.5 - Class 1/R DF = 0.72

>2.5 - Class 2/S, DF = 0.3

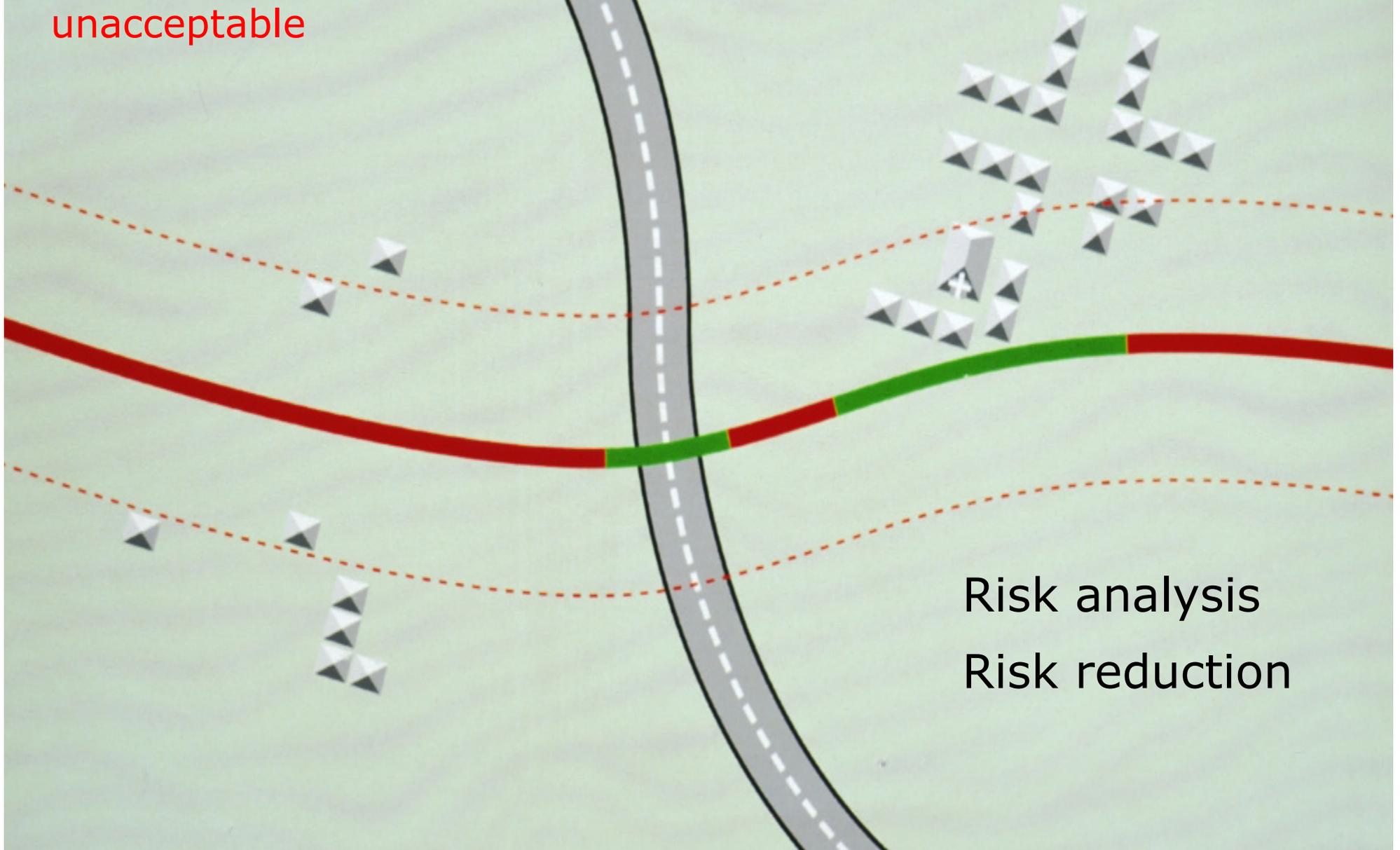
Pipeline Design and Risk Management



Pipeline is no longer
code compliant

Risk to people may be
unacceptable

Pipeline Risk Management



Risk analysis

Risk reduction



Distance from pipeline

UKOPA – RA Issues & Initiatives

Issues

- Risk Assessment methodology
- Recommended inputs and assumptions
- Recommended criteria and mitigation measures
- Consistency in results and decisions

Initiatives

- Industry expert group – open discussions with HSE
- Pipeline Fault Database and published failure data
- Technical studies
- Development of pipeline code supplements – publication of pipeline fault data and results of studies

The Role of Engineering Codes

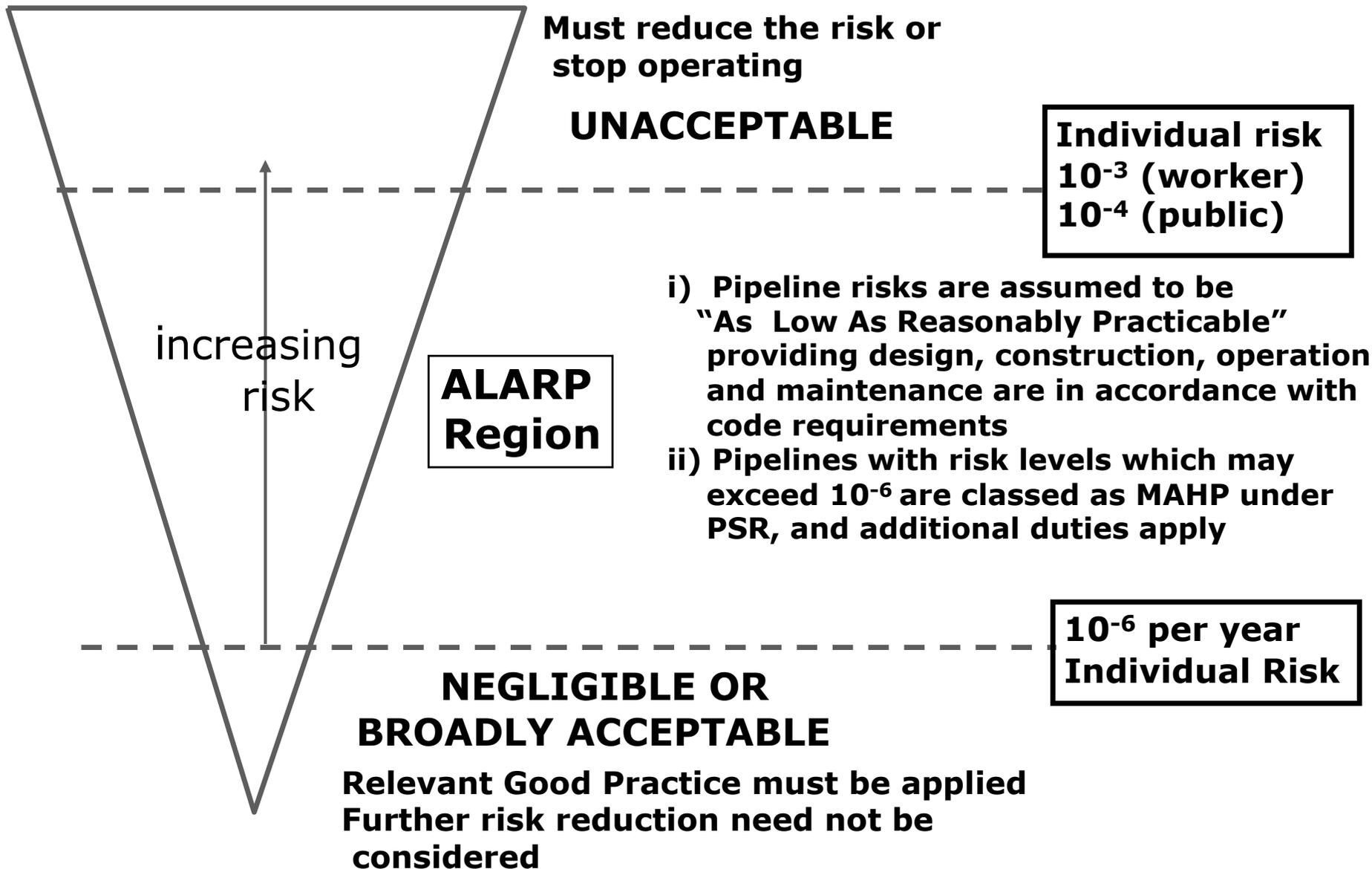
- Proceduralise the application of engineering principles in a safe, validated manner
- The use and application of recognised codes is a prerequisite for compliance with safety legislation
- Approved standards are used to set safety standards

UK Pipeline Codes

Prior to major pipeline development in the UK (mid 60s) UK pipeline codes were simple interpretations of American ASME Codes

UK codes were developed to establish more rigorous safety standards for pipelines in more densely populated land:-

- i) Area classification and routing to avoid population
- ii) Use of BPD – minimum separation distance between pipeline and surrounding population
- iii) Stress limits (design factor)
- iv) Testing requirements (level and length)
- iv) Increased precautions to minimise risk of failure (depth of cover, increased wall thickness, protection)
- v) Requirements for surveillance, monitoring and inspection to detect and repair damage
- vi) Requirements for monitoring route and managing changes in risk



Why Codify Risk Assessment?





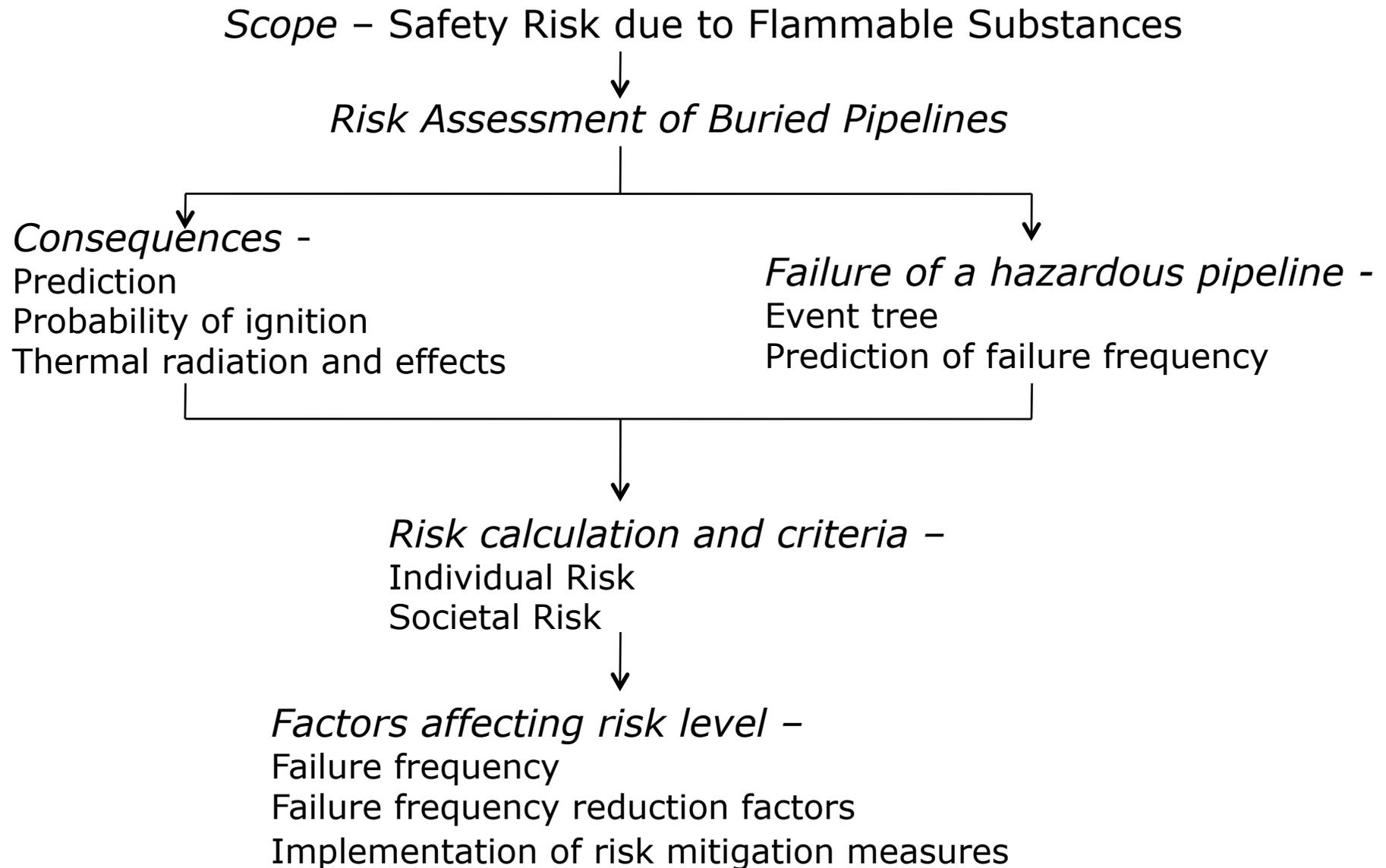
***IGE/TD/1 Edition 4 Supplement 2
Communication XXXX***

***APPLICATION OF PIPELINE RISK ASSESSMENT TO PROPOSED
DEVELOPMENTS IN THE VICINITY OF MAJOR HAZARD PIPELINES –
HIGH PRESSURE GAS PIPELINES***



**Code of practice for pipelines –
Part 3: Guide to the application of pipeline risk assessment to proposed developments in
the vicinity of major hazard pipelines containing flammables – Supplement to PD 8010-1:2004**

TD/1 and PD 8010 Code Supplements - Structure



TD/1 and PD 8010 Code Supplements - Structure

Supporting Appendices/Annexes:-

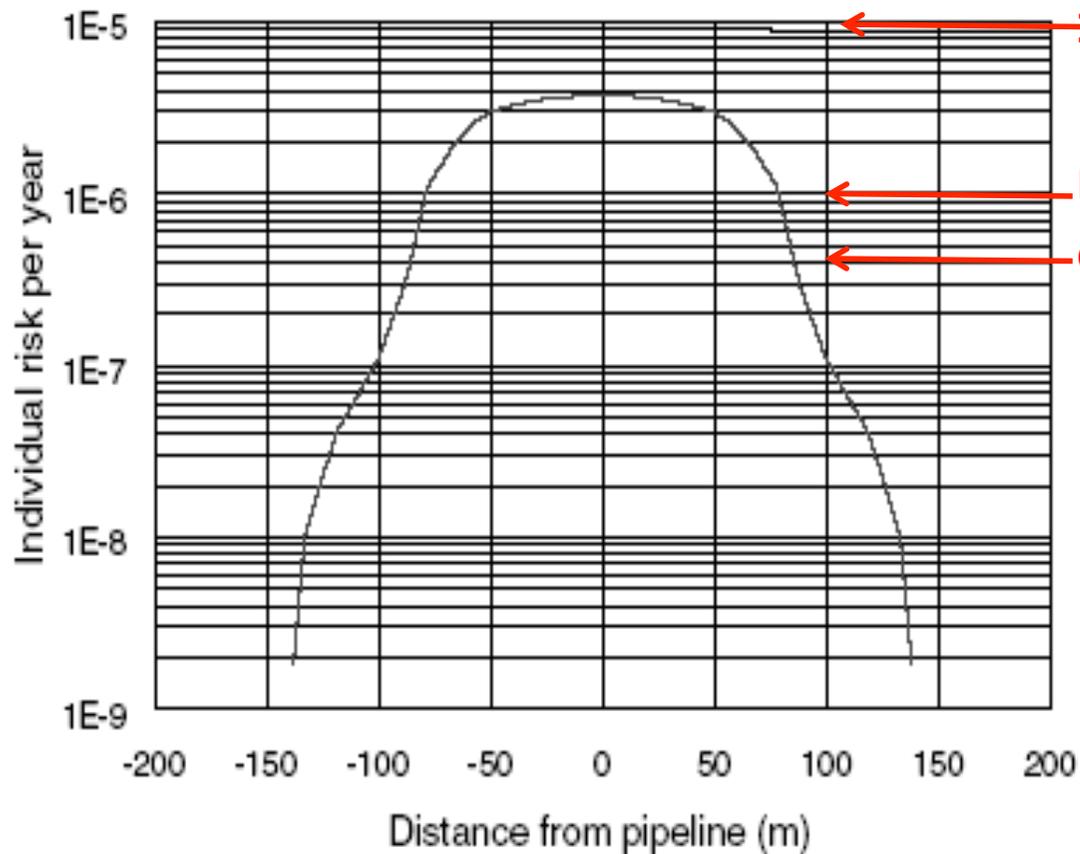
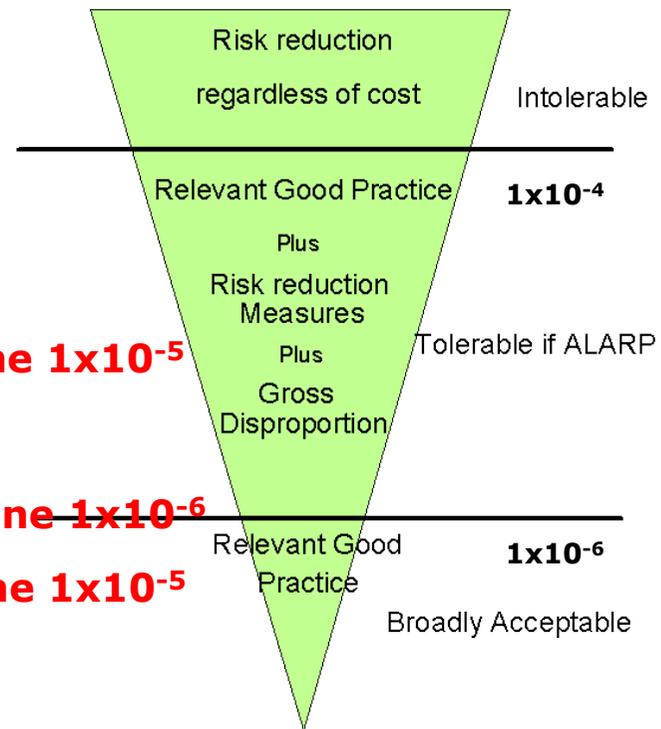
- Summary of HSE methodology for provision of LUP advice
- Failure Frequencies for UK Pipelines
- Example of site specific risk assessment
- Benchmark cases

Some Key Features:-

- Risk Criteria – Individual and Societal
- Guidance on pipeline specific failure frequencies based on current UKOPA data

Individual Risk Criteria

Figure 1: Types of ALARP Demonstration



Societal Risk Criteria:-

TD/1 Supplement:-
Refers to existing Figure 20

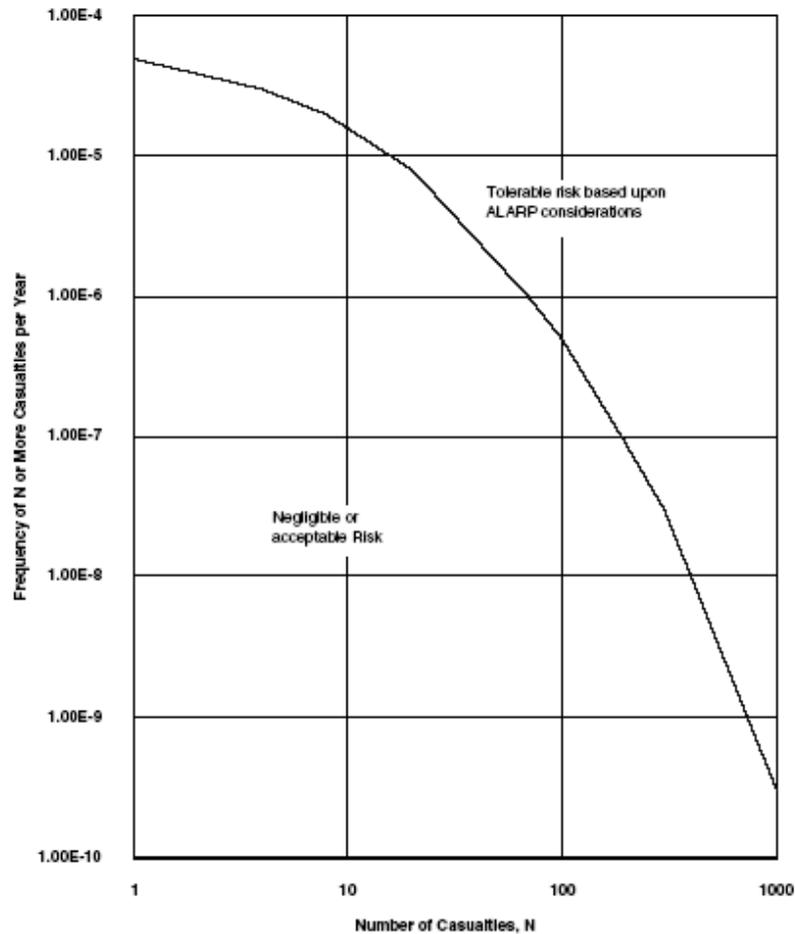
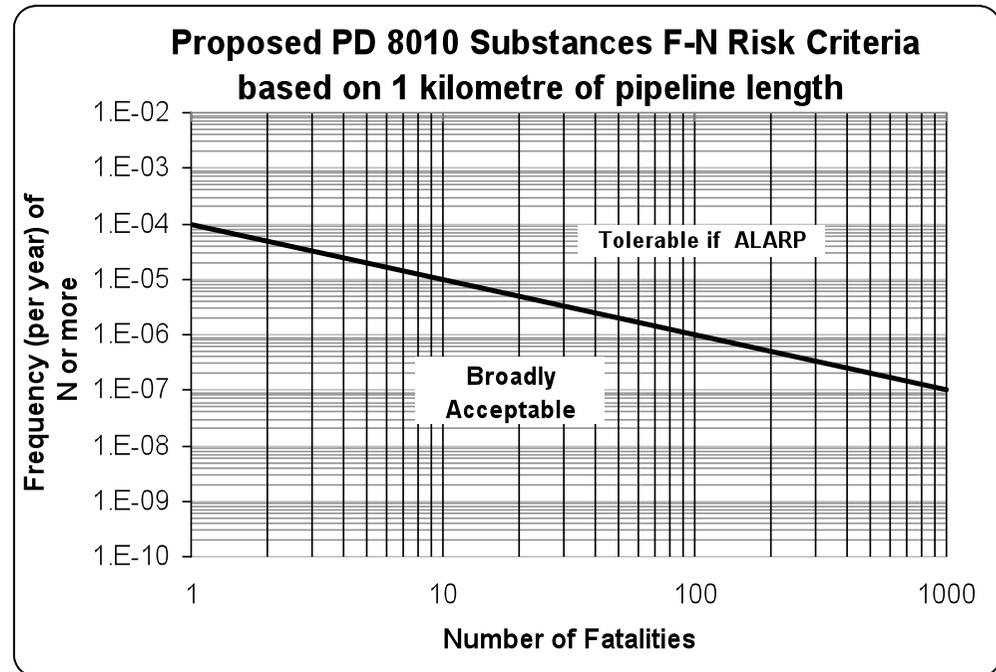


Figure 20 - Sample FN criterion (based on extensive application of previous editions of IGE/TD/1)



PD 8010 Supplement –
includes new FN Curve

UKOPA Failure Data

Damage Mechanism	Total Failure Rate (1000 key)	% Total	% Pin	% Hole	% Rupture
3 rd Party	0.057	21.6	2.3	15.2	4.2
External Corrosion	0.046	17.4	13.3	3.4	0.8
Internal Corrosion	0.003	1.1	1.1	0.0	0.0
Material & Construction	0.076	28.8	23.9	4.9	0.0
Ground Movement	0.009	3.4	1.1	1.5	0.8
Other	0.073	27.7	19.7	7.2	0.8
Total	0.264	100.00	61.4	32.2	6.4

Guidance on Failure Frequencies of UK Pipelines in Supplements

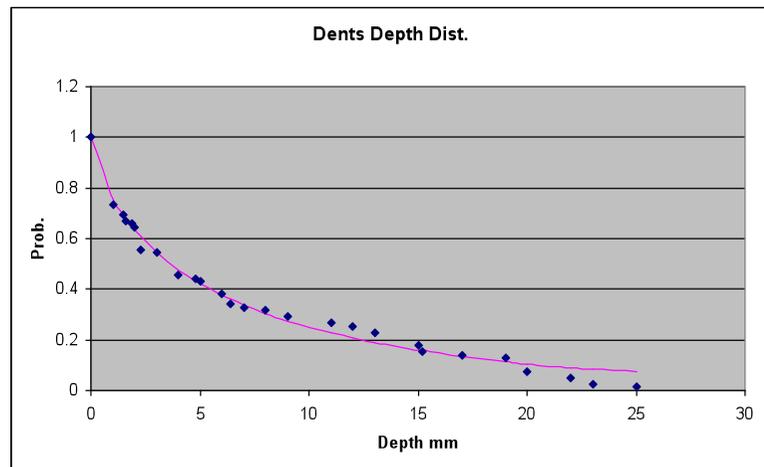
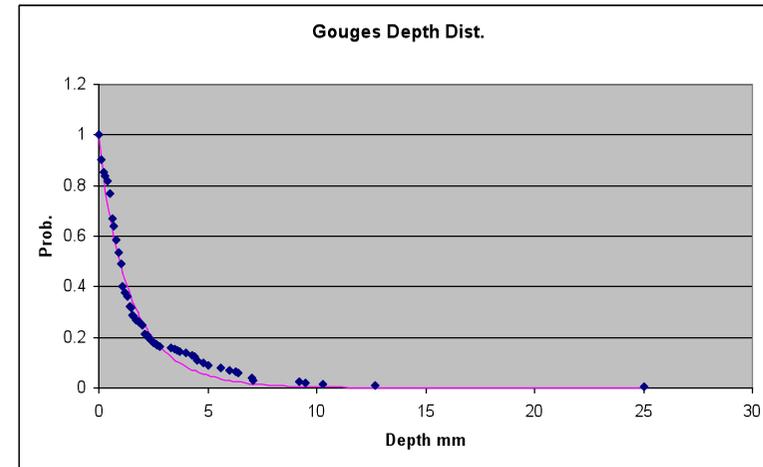
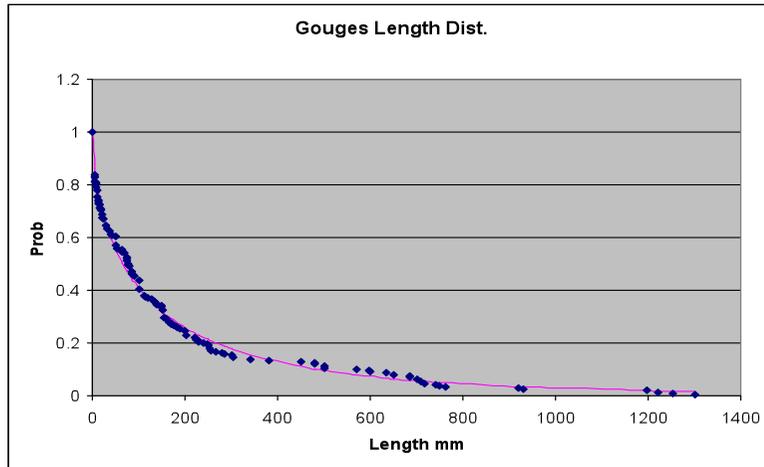
- 3rd Party – Random, use predictive approach
- External corrosion – dependent on wall thickness and age (guidance included)
- Material and Construction – dependent upon wall thickness and age (guidance included)
- Ground movement – depends upon susceptibility to natural landsliding – recommended background rate – 2.1×10^{-4} per 1000 km-y

For the above damage mechanisms, the supplements include specific guidance for derivation of pipeline specific failure rates

Prediction of Failure Frequency due to 3rd Party Interference

- Failure data is sparse
- Damage mechanism is random
- Failure is dependent upon wall thickness, pressure, diameter, material properties etc
- Reduction factors for wall thickness, design factor, depth of cover, slabbing and surveillance are included
- Recommended predictive tool is FFREQ
- Simple guidance is provided to allow users to determine conservative estimate for a specific pipeline

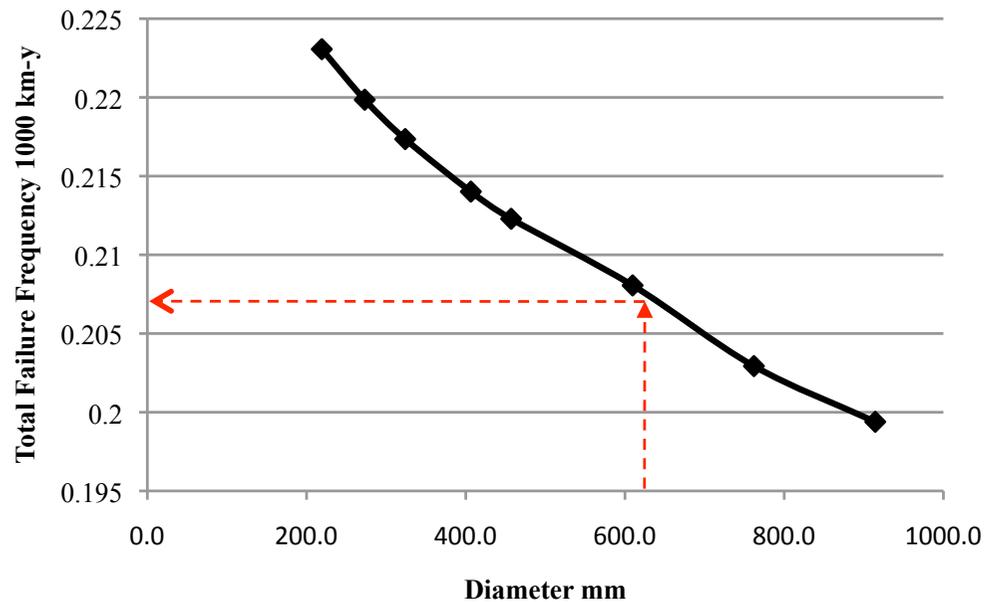
UKOPA Fault Data Statistics



Probability of getting a dent
/gouge fault of certain size

Simple Guidance on Estimation of 3rd party Failure Frequency

Generic Failure Frequency Curve



Curve based on:-

Maximum design factor – 0.72

Minimum wall thickness 5mm

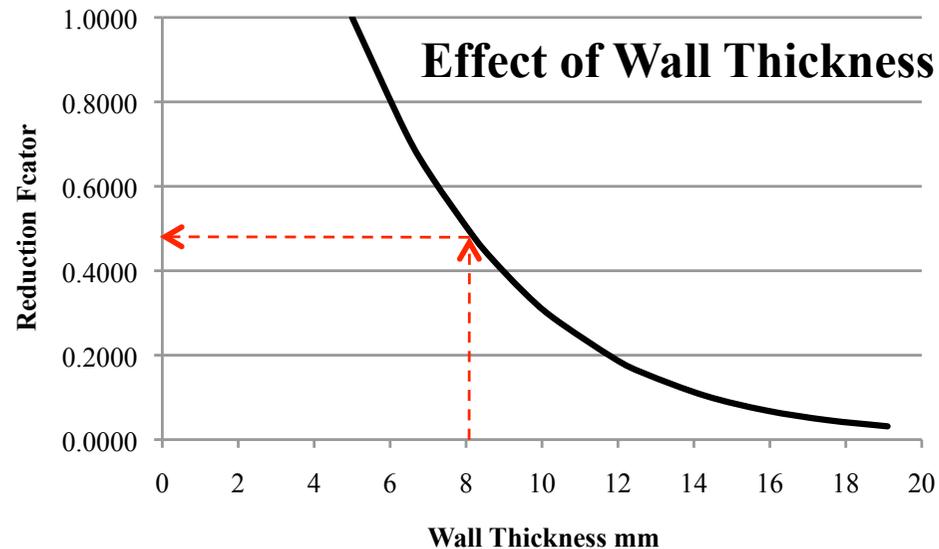
High grade (X65)

Minimum toughness

Failure frequency for
610 mm diameter pipe
= 0.208 per 1000km-y

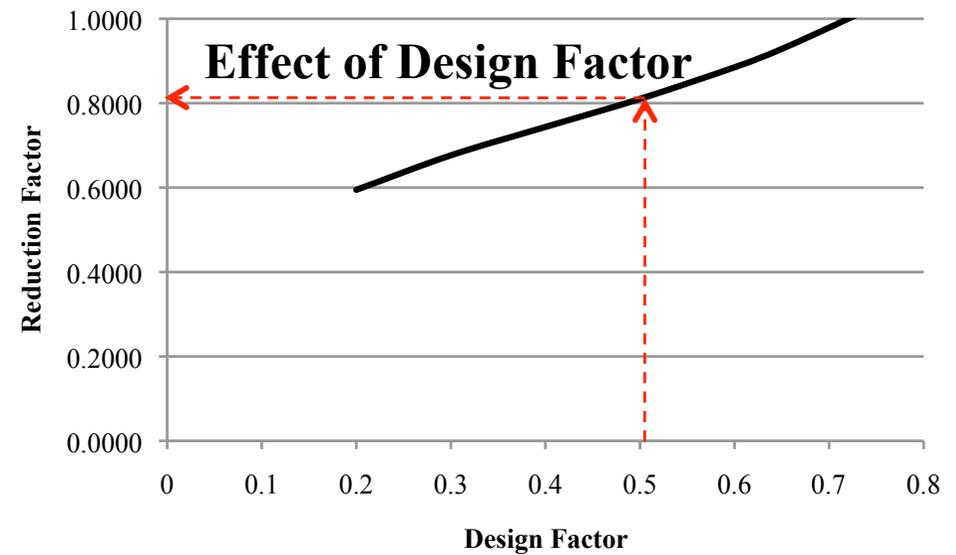
Example – estimate failure frequency for 610 mm diameter, 9.5mm wall thickness pipe operating at a DF = 0.5

Reduction factors for Wall Thickness and Design Factor



Reduction due to wall thickness of 7.9mm = 0.5

Reduction due to design factor of 0.5 = 0.81



Estimated total failure frequency for 609mm diameter 7.9mm wall thickness pipe operating at design factor 0.5 is:-

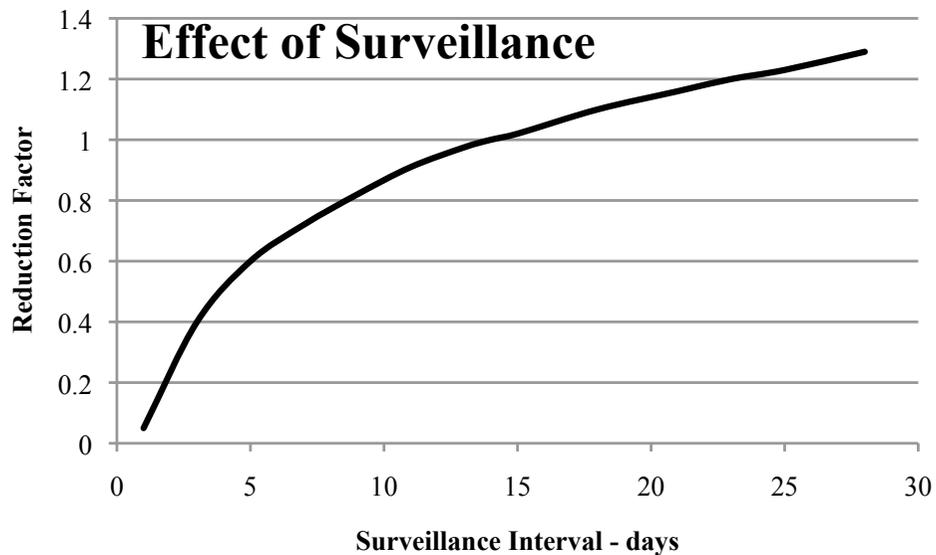
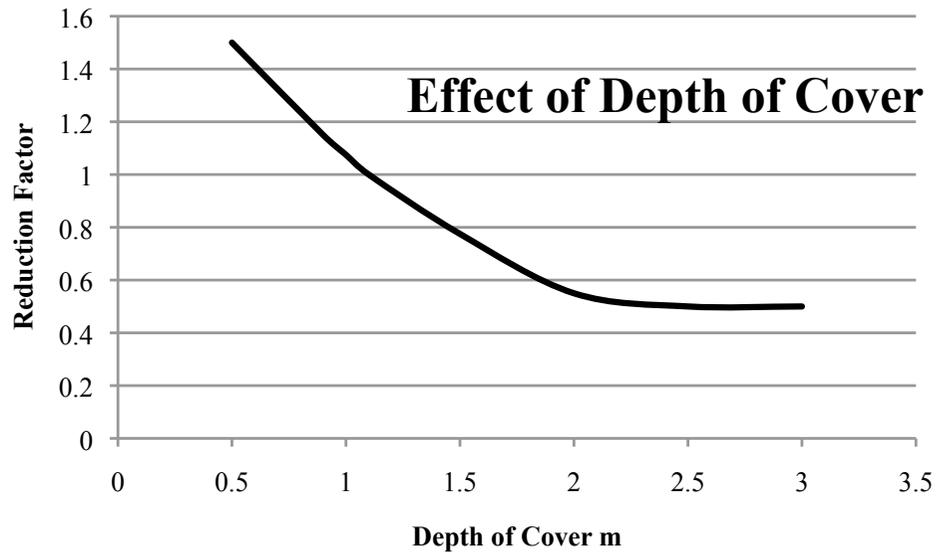
Total Failure Freq = $0.208 \times 0.5 \times 0.81 = 0.084$ per 1000 km-y

Of which 0.7 of rate is conservatively assumed to be due to ruptures

Comparison with FFREQ:-

Pipe Case	Estimated total FF	FFREQ prediction	Estimated rupture freq	FFREQ Rupture freq
609mm dia, 7.9mm wt, df = 0.5	0.084	0.061	0.059	0.02

Other Site Specific Reduction Factors:-



Protection Measure	Reduction Factor
Concrete slab	0.16
Concrete slab + visible marking	0.05

The pipeline specific failure frequency is reduced further through the application of mitigation measures:-

Eg - depth of cover – 2m and installation of concrete slabbing with visible marking:-

Failure freq – $0.084 \times 0.5 \times 0.05 = 2.1 \times 10^{-3}$ per 1000 km-y

Further reduction in failure frequency due to more frequent surveillance may be appropriate in some circumstances

Role of the UK Pipeline Codes PD 8010 and IGE TD/1

- Compliance with PD 8010 (all substances) and IGE TD/1 (natural gas) demonstrates compliance with PSR 96.
- Compliance with the above pipeline codes demonstrates that the risk is **As Low As Reasonably Practicable** (ALARP).
- Supplements will ensure above principles extend to the application of pipeline QRA in the management of pipeline risks and land use in the vicinity of MAHPs

Development of Code Supplements

- **Purpose** - to provide a codified approach to pipeline risk assessment for use by all stakeholders
- **Aim** - to ensure a standard and consistent approach and reduce potential for technical disagreements and inconsistencies in results and decision making
- **Objectives** - to provide authoritative and accepted guidance on :-
 - site specific risk assessment (wall thickness, depth of cover, damage mechanisms and failure frequency)
 - Application and effect of risk mitigation measures
 - Establish the means of recording, publishing and developing best practice

Strategy for Development

- Common for BSI & IGEM
- Joint technical working group:
 - First draft (based on natural gas)
 - Parallel development of code supplements
- Separate public consultation
- Co-ordinated publication programme

The Standards Bodies defined a series of structured consultation, acceptance and revision steps to ensure successful publication of the code supplements

Risk Assessment Code Supplements – Current Status

- Drafting is complete
- Public comment has been received and addressed
- Documents are finalised
- Publication is planned for July 2008