

Managing Fatigue in an Onshore Pipeline System

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Agenda

Background

Managing Fatigue

Testing and Inspection

Data

Analysis

Case Study

Conclusions

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P E N S P E N

- 3 Casualties
 - Mechanical damage plus cyclic pressure load
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- 7 hectares contaminated
 - Seam weld anomaly plus cyclic pressure load

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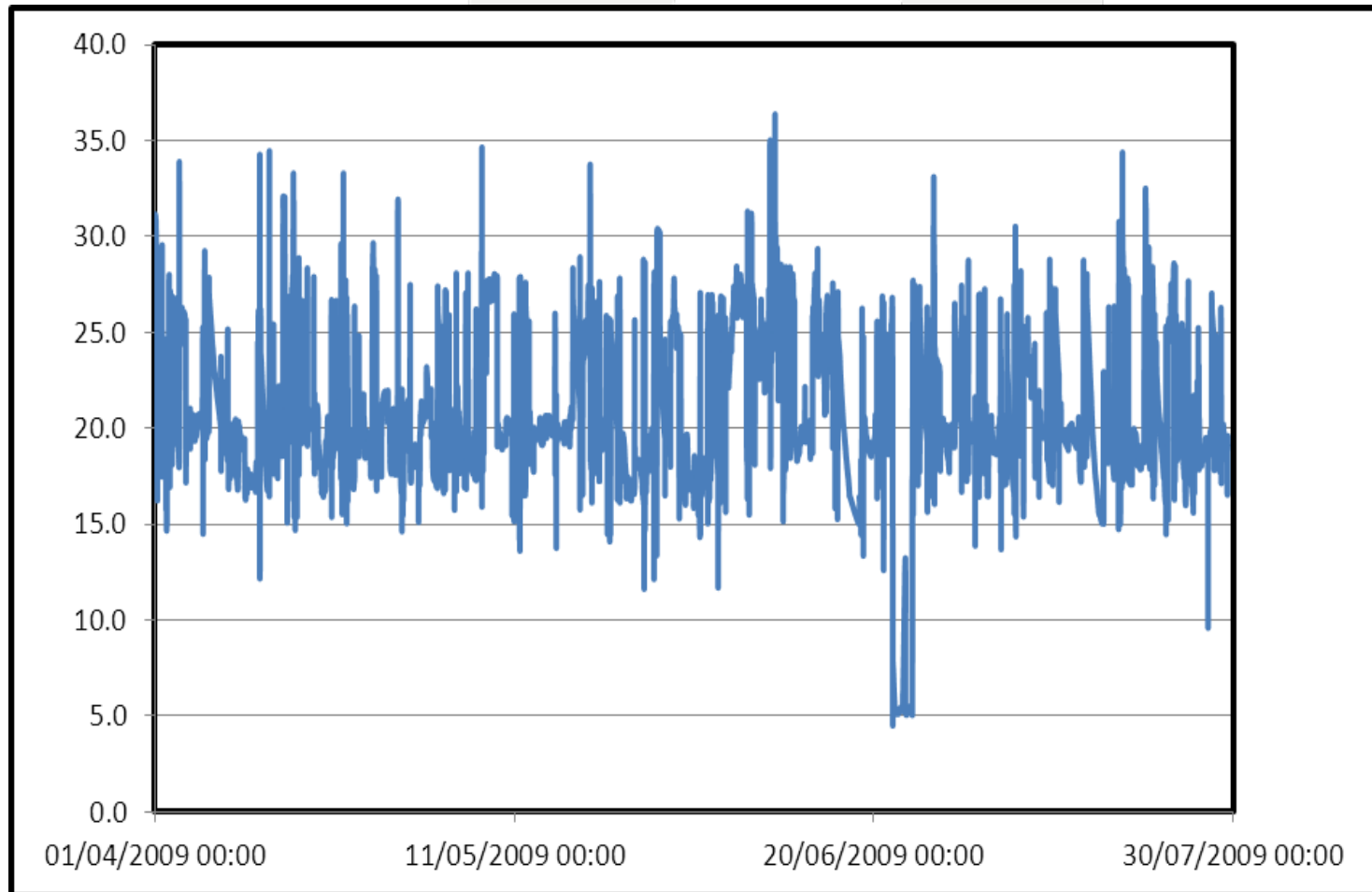
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- Fatigue loading is mainly a problem for pipelines transporting liquids.

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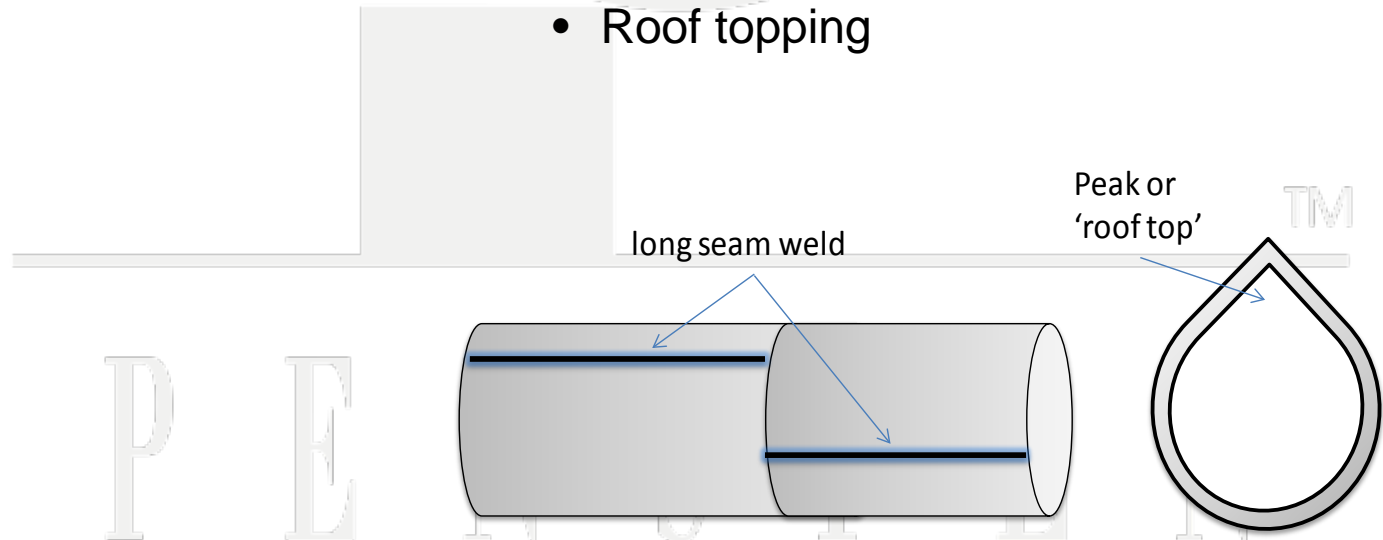
- Crude oil pipeline pressure history



- Gas pipeline pressure history



- When is fatigue a concern?
 - Significant pressure cycles
 - Stress concentrating features
 - Weld anomaly
 - Hook crack
 - Dent
 - Roof topping



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- Requirements for Managing Fatigue
 - Awareness
 - Information on stress concentrating features (weld defects etc.)
 - Pressure data
 - Reliable analytical models for:
 - Critical defect sizes
 - Crack growth

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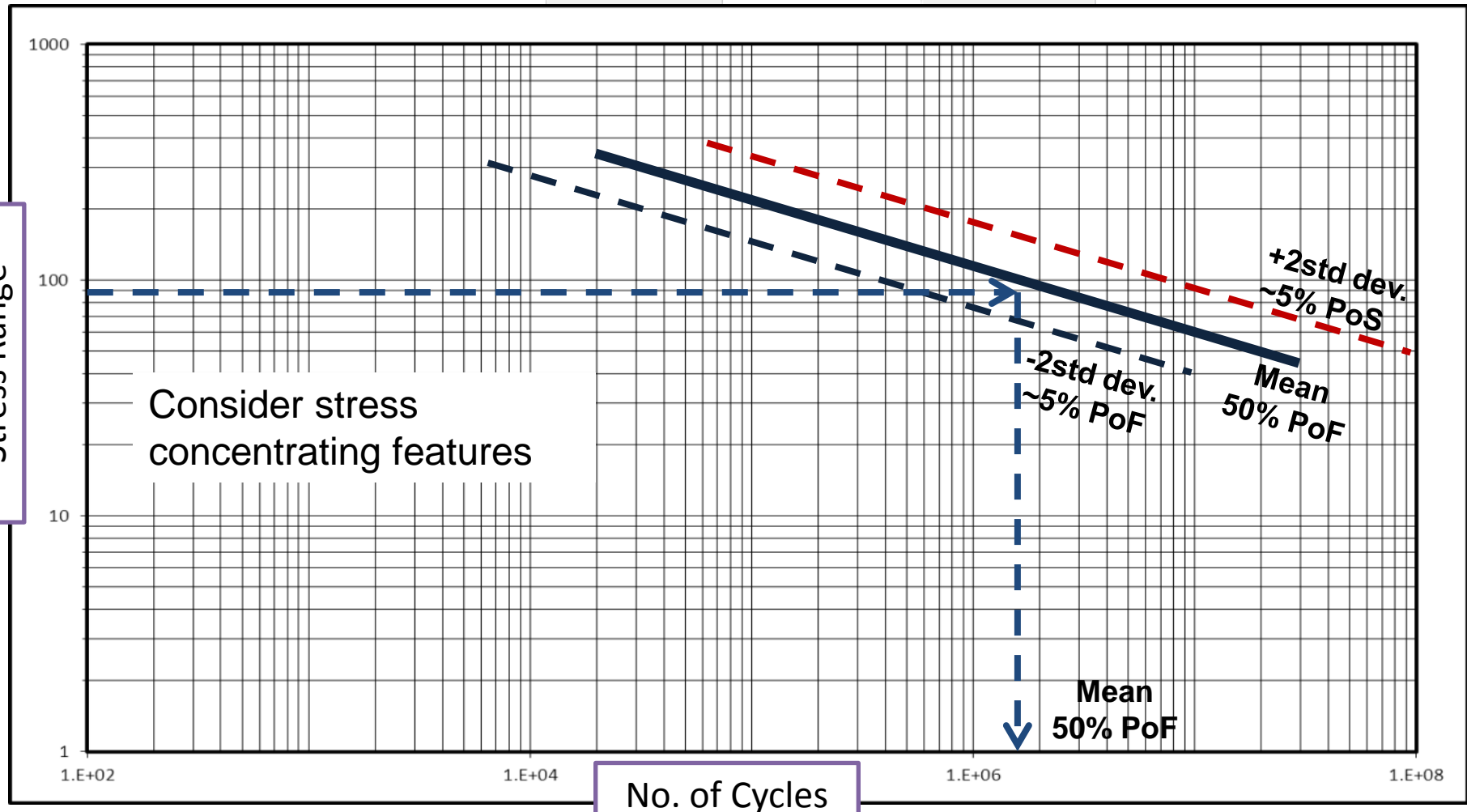
- Awareness - Failures
 - Enbridge 2011
 - SPSE 2011
 - Others...



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- Awareness – Design checks
 - Evaluation of expected fatigue performance can be completed using SN.



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- Hydrotesting
 - Will find (fail) critical defects

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- Inspection
 - Ultrasonic Crack Detection and EMAT tools
 - Sizing remains difficult
 - Unusual seam welds can mask defects





- Inspection
 - High resolution geometry tools
 - Dent strain
 - Dent shape

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- Pressure Data
 - High frequency
 - Time stamped
 - Upstream
 - Downstream
 - Understanding of hydraulic profile
 - Interpolation to estimate pressure at defect location

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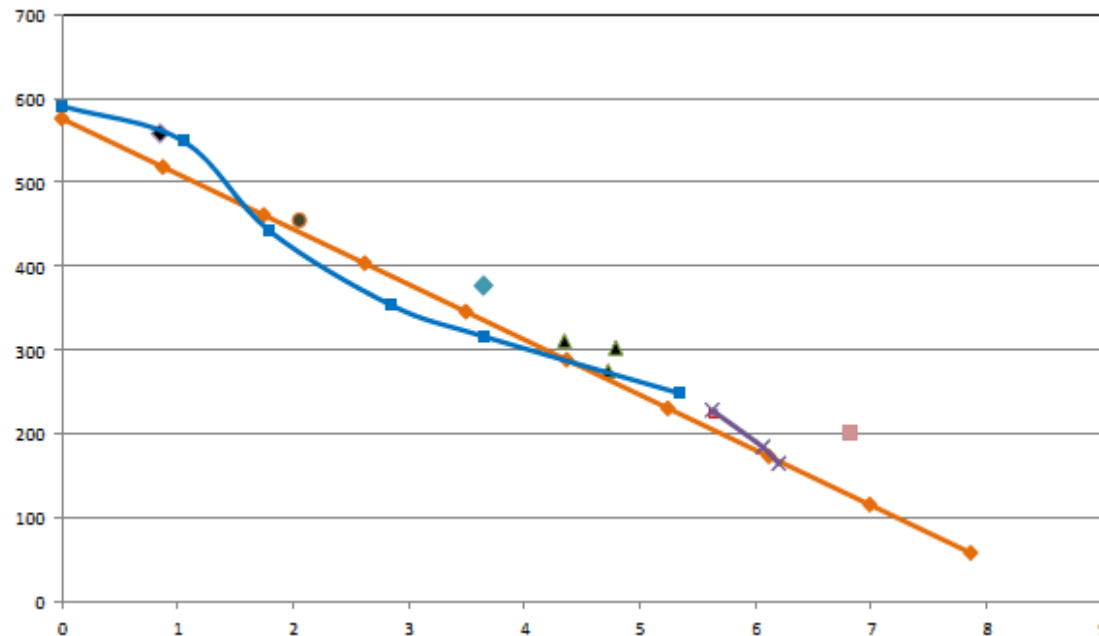
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- Analysis of Weld Defects
 - Critical defect size
 - Toughness?
 - Strength?
 - Crack?
 - Brittle or ductile failure behaviour?
 - Crack growth rates
 - Stress concentrating features
 - Roof topping
 - Misalignment

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- Testing of cracks in SAW welded pipe indicates that failure is ductile and predicted by standard equations



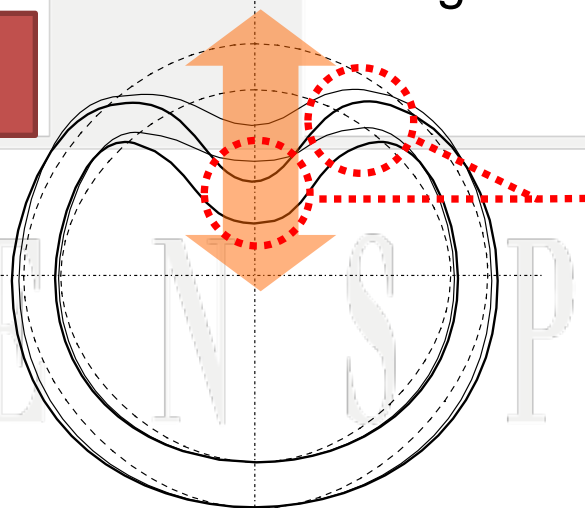
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- Recommended approach for weld defects
 - Pipelines a relatively thin, ductile material (weld zones are also generally ductile), operating at normal temperatures.
 - Critical defect sizes should be calculated using standard pipeline methods (NG-18). Testing can be used to confirm this.
 - Fatigue crack growth rates should be calculated using standard fracture mechanics methods (BS 7910). Careful consideration should be given to stress concentrating features.

- Recommended approach for dents
 - Check dent strain (ASME B31.8)
 - Depth based fatigue assessment
 - Consider constraint conditions
 - FEA to estimate stress concentrations followed by SN based fatigue.

the dent depth changes as the internal pressure changes



cyclic internal pressure induces cyclic stresses and strains in the dent

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- Case Study

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Pipeline System

Pipeline	Nominal outside diameter Inches	Type of Pipe	Material API Grade	Thk. mm	MAOP Bar	Comm. Date
ERW#1	10	ERW	X 52	4.8	79	1981
ERW#2	14	ERW	X 60	5.6	88.5	1985
ERW#3	12	ERW	X 60	5.4	88.5	1992
Seamless#1	6	Seamless	Grade B	5.6	99.3	1962
Seamless #2	12	Seamless	X42	6.35	71.5	1962
Seamless#3	10	Seamless	X 52	6.35	82.7	1969

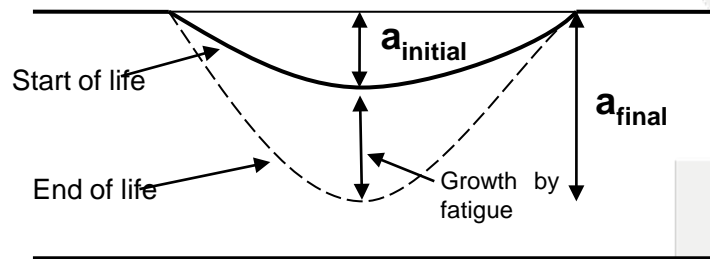
- Awareness – 20 years ago
 - MFL inspections
 - Dents not reported
 - Gouges difficult to detect
 - Seam weld defects not detectable
- Pressure records available
- Evidence of failures around the world.

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- 1994 first fatigue study on the Esso System.
- No data was available on seam weld anomalies.
- Remaining fatigue life calculated by:



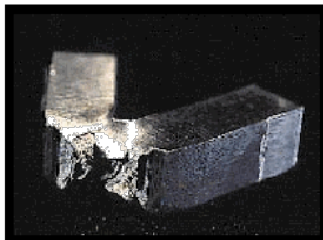
$a_{initial}$ = initial defect size
 a_{final} = final defect size
 a_{final} = final defect size

- Calculating the largest crack type defect that would have survived the pipeline's pre-commissioning hydrotest ;
- Determining the smallest defect which would fail at the pipeline's MAOP; and,
- Calculating the time for the defect to grow from its hydrotest survival size to the its MAOP failure size.



- Results
 - 3 pipelines predicted to have exceeded their design fatigue life
 - Hydrotest recommended
- Review
 - Assumption on initial defect conservative and did not include consideration of credible defects.
 - Limited pressure data (1 week).
 - Dents not considered.

- 1995 further study
 - Defect credibility
 - Measured material properties
- Results
 - 2 pipelines still exceeding 'design' fatigue life
- Review
 - Dents not considered



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- 1999 Transverse Field Inspection for seam weld anomalies
 - No crack like anomalies reported
 - Detection threshold is high – significant defects could be missed.



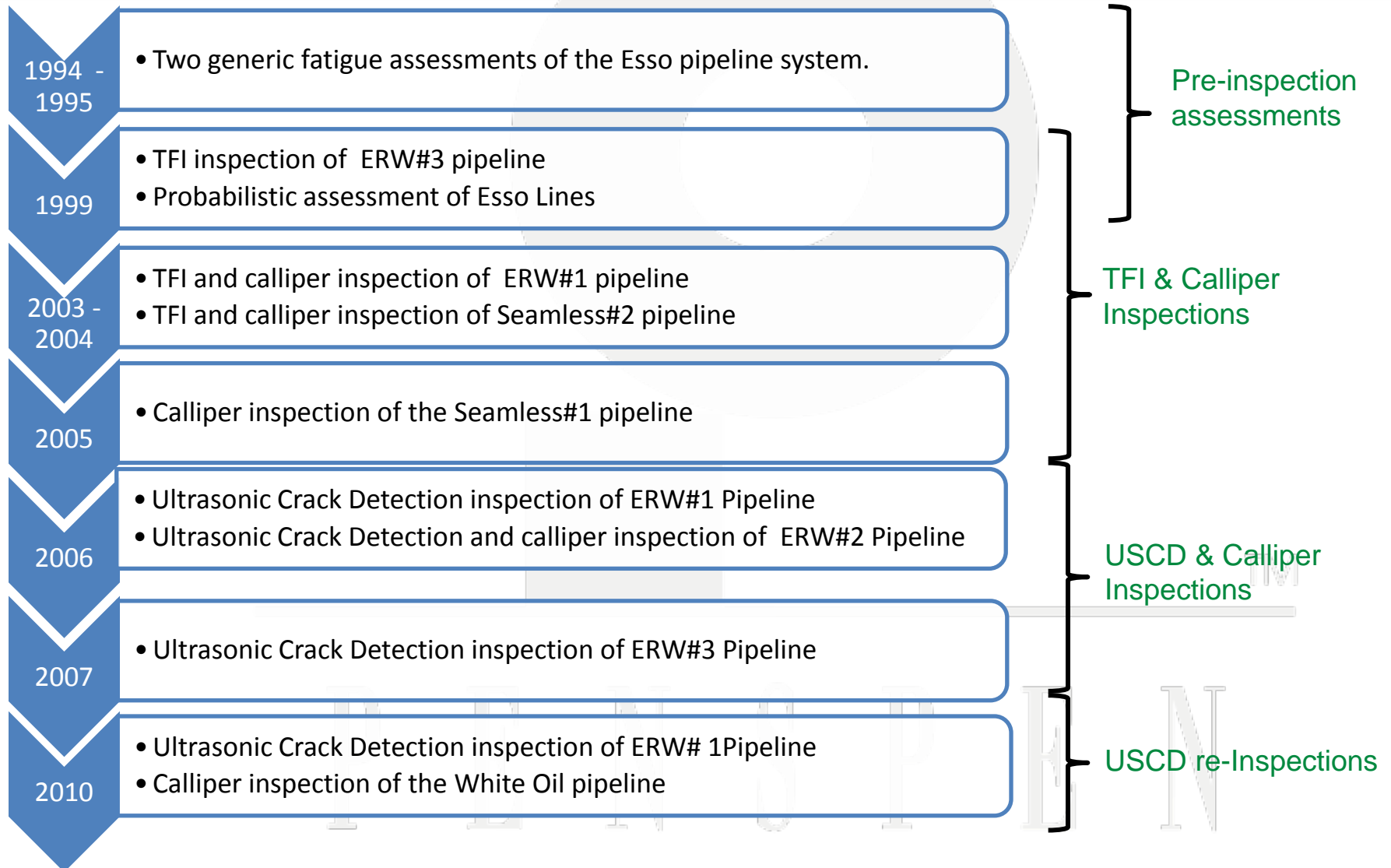
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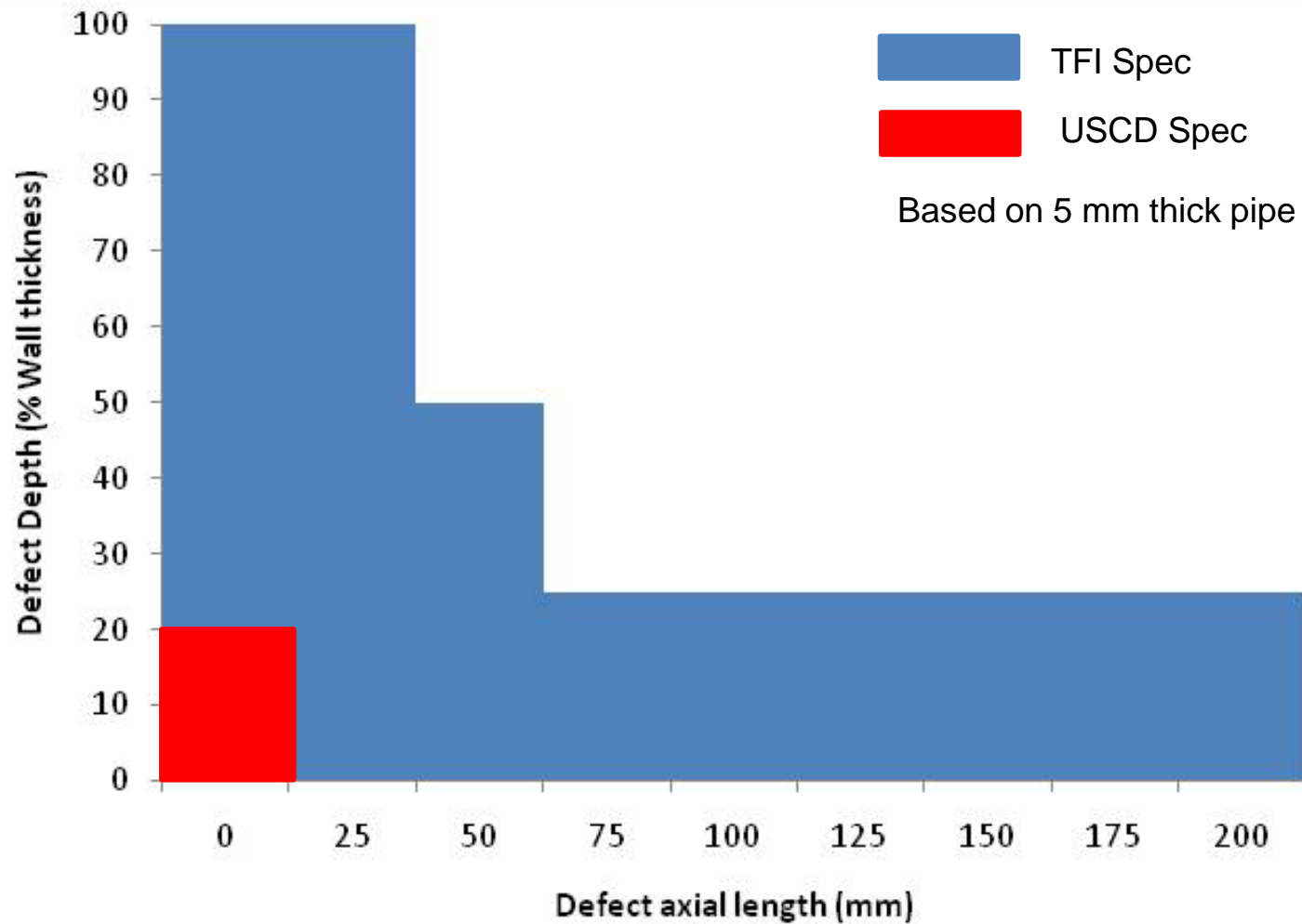
- 1999 further studies
 - Fatigue study on inspected line assuming defect at limit of detection.
 - Probabilistic study of other lines
- Results
 - Fatigue life of inspected pipeline extended to 2008
 - 20% probability of failure due to fatigue estimated for other line.™
- Review
 - Dents not considered

- 1994, 1995, and 1999 studies were generic, and relied on assumptions due to lack of data.
- Internal inspection specifically looking for seam weld anomalies in 1999. Since then all the pipelines in the Esso system have been inspected for fatigue-sensitive defects
- All inspections were followed by engineering assessments





- Initial inspections for seam weld anomalies were carried out using TFI
- TFI
 - Detection threshold ~20% wt and 'open'
- USCD
 - Detection threshold 1 mm depth for defects longer than 25 mm
- Since 2006 all inspections looking for seam weld cracks have been USCD



- Comparison of results of TFI and USCD inspections

Inspection Technology	TFI	USCD
Inspection Year	1999	2007
Findings	No Crack-like anomalies	42 Crack-like 148 notches 252 Weld anomalies

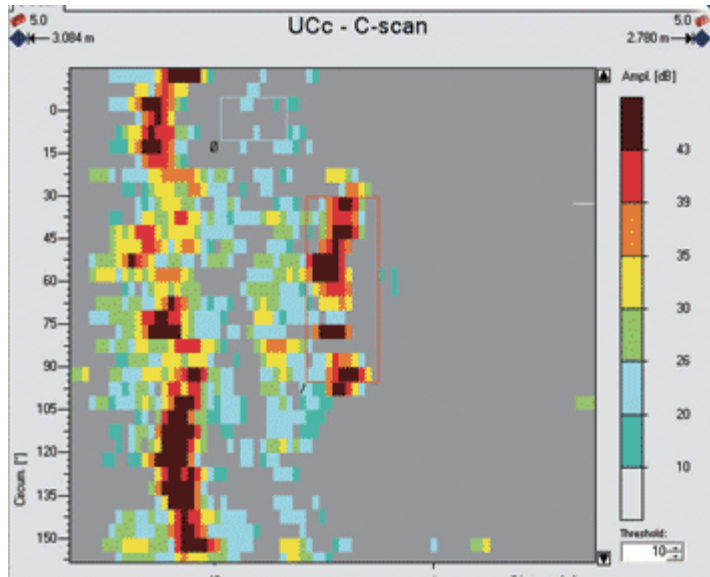


- USCD tools are sensitive to a variety of anomalies. The following anomaly categories are often reported
 - Crack-like
 - Crack-fields
 - Weld Anomalies
 - Mill Anomalies
 - Notch-like



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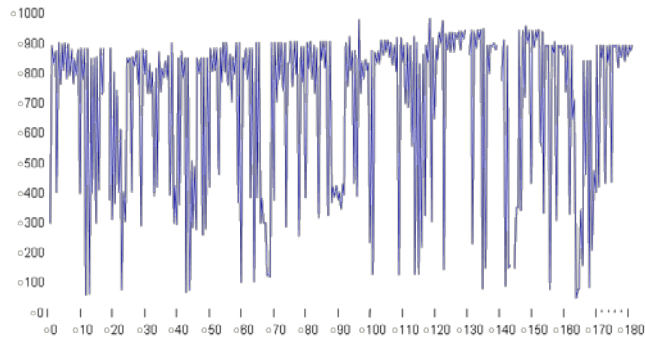


- Crack-like anomalies and weld anomalies are the most susceptible to fatigue.
- Notches and mill anomalies are less susceptible.
- Classification of anomalies is critical.
- The operator relies on competent ILI data-analysis.

- 2006 data

	Crack Fields	Crack - Like	Notch Like	Not Decidable
N° Reported	6	1,857	5,549	140

- 93 digs and associated repairs
- 11% of crack-type defects actually contained planar anomalies
- 2% of defects in which the USCD had not detected crack-like anomalies were found to actually contain planar defect types



- Pressure Data

- 1994 study used one week of pressure data
- 2003 to 2007 assessments used 1 year of pressure data
- Recent assessments used 9 years of pressure data
- Pressure now recorded every 2 minutes.

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BRITISH STANDARD

Guide to methods for
assessing the
acceptability of flaws in
metallic structures

BS 7910:2005
*Incorporating
Amendment No. 1*

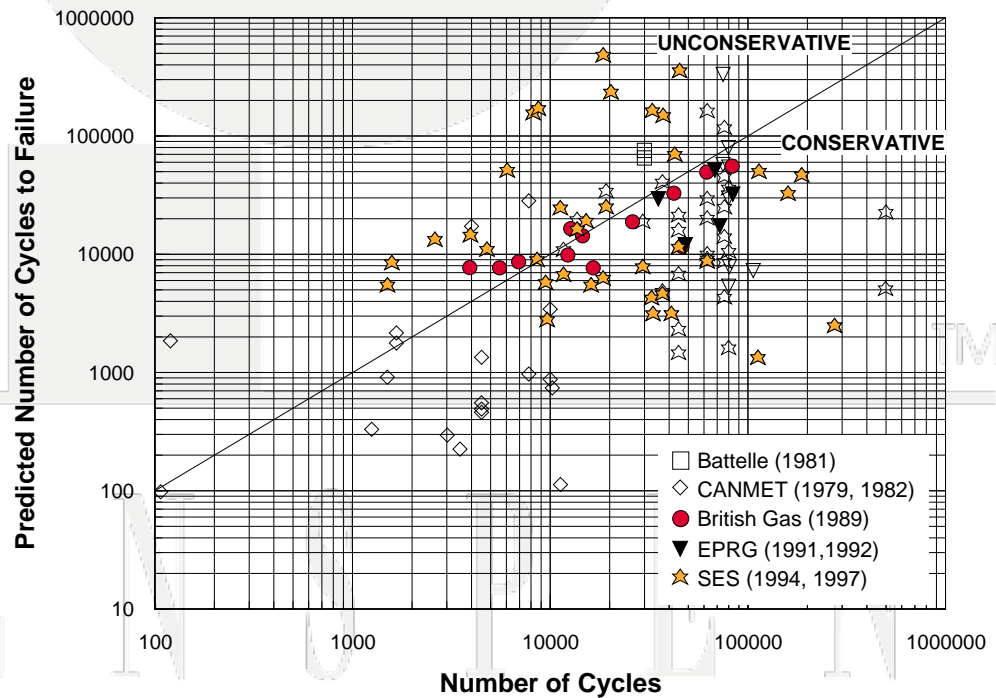
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BSI
British Standards

- Assessment - Cracks
 - BS 7910, recommended in PDAM
 - Conservative
 - Assessments generally predict numerous defects to have already failed
 - However no fatigue induced failures have occurred to date
 - Sources of conservatism
 - Correlation between Charpy impact strength and true material fracture toughness.
 - Fatigue crack growth rates, which are known to be a “upper-bound” estimate.

- Assessment – Dents
 - EPRG recommended in PDAM
 - Conservative due to genuine variance in the test data





- Future management - Inspection
 - Continue multiple technology inspection regime
 - Understanding & supporting latest technology for inspection
 - Cooperation with ILI companies to improve classification of defects – reduce bias

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- Future Management – Operation
 - Better understanding of pipeline operation – reduce pump & valve transients, and unnecessary fatigue loading of pipeline.
 - Education of operating staff on fatigue (development of operating philosophy).
 - Pressure transient analysis of system to assess anomalies to local pressure rather than inlet or outlet pressure.
 - Communication/MoC ensure operational changes are communicated.



- Future Management – Assessment

- Material (ring) testing to get better understanding of fatigue susceptibility and critical defect sizes
- Correlation of successive inspections to infer dent dates and crack growth.
- Promoting awareness of fatigue in the pipeline industry – pipelines are getting older



Thank you

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